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Integrated Design and Analysis Overview

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3rd Gen Airframe/TPS:

Integrated Design and Analysis

♦ **PMC Damage Tolerance & Repair**

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♦ **Safe Structures Design Technologies**

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3rd Gen Airframe/TPS:

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PMC Damage Tolerance and Repair Goals & Objectives

- ◆ Develop methodology for assessing the effects of manufacturing defects
- ◆ Develop damage tolerance criteria and damage tolerance database for RLV cryogenic tank structures
 - impact
 - pressure leakage
 - cryogenic permeation
 - validated damage prediction tools
- ◆ Develop repair technology

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PMC Damage Tolerance and Repair Current Program Status

- ♦ Initiated in FY1999 as Bantam Damage Tolerance Program
- ♦ Continued as PMC Damage Tolerance Program during FY2000 with reduced funding level
- ♦ Needs continuation to address technology issues that will limit composites application to cryogenic tank structures

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PMC Damage Tolerance and Repair

Current Technical Status

◆ FY1999:

- Established damage tolerance requirements (impact, pressure leakage, cryogenic permeation)
- Fabricated and impact tested flat and curved thin-skin panels made of different material forms
- Conducted impact damage tolerance tests for damage resistance and barely visible damage (BVID); developed a 0.05 in. dent depth BVID criterion
- Developed analytical methods to predict the impact response and damage resistance for curved, thin laminated composites

◆ FY2000:

- Assessed existing repair methods for stiffened-skin and sandwich constructions
- Developed analysis methods for optimally sizing bolted and bonded anisotropic patch repairs
- Completed compression-after-impact strength tests on three material forms
- Developed analytical models and methods to assess the critical size of delaminations for combined loading conditions
- Assessed mixed-mode fracture toughness for IM7/977-2 and AS4/PEEK material systems at cryogenic temperatures
- Conducting pressure leakage threshold tests

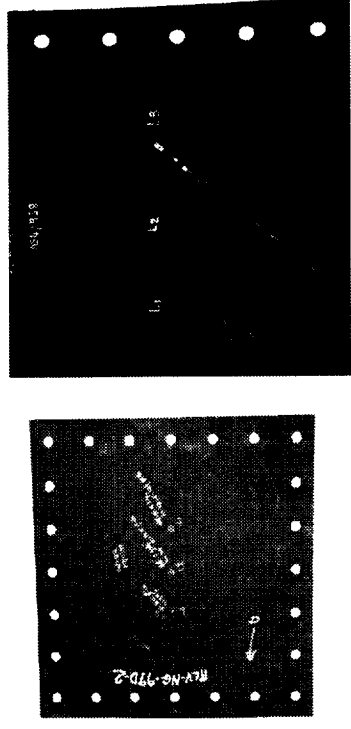
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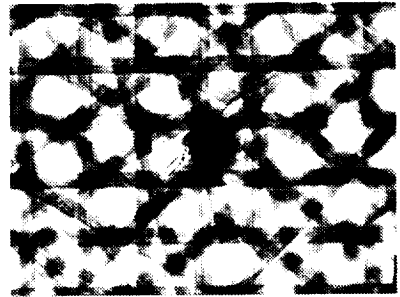
PMC Damage Tolerance and Repair

ENERGY THRESHOLDS FOR BARELY VISIBLE IMPACT DAMAGE OF CURVED THIN LAMINATES MADE OF DIFFERENT MATERIAL FORMS

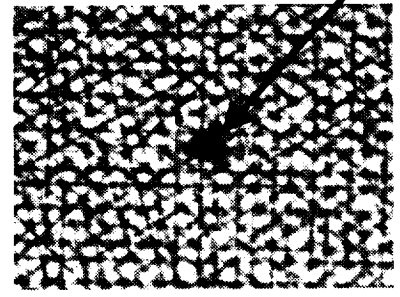
Criterion: 0.05-in. dent depth



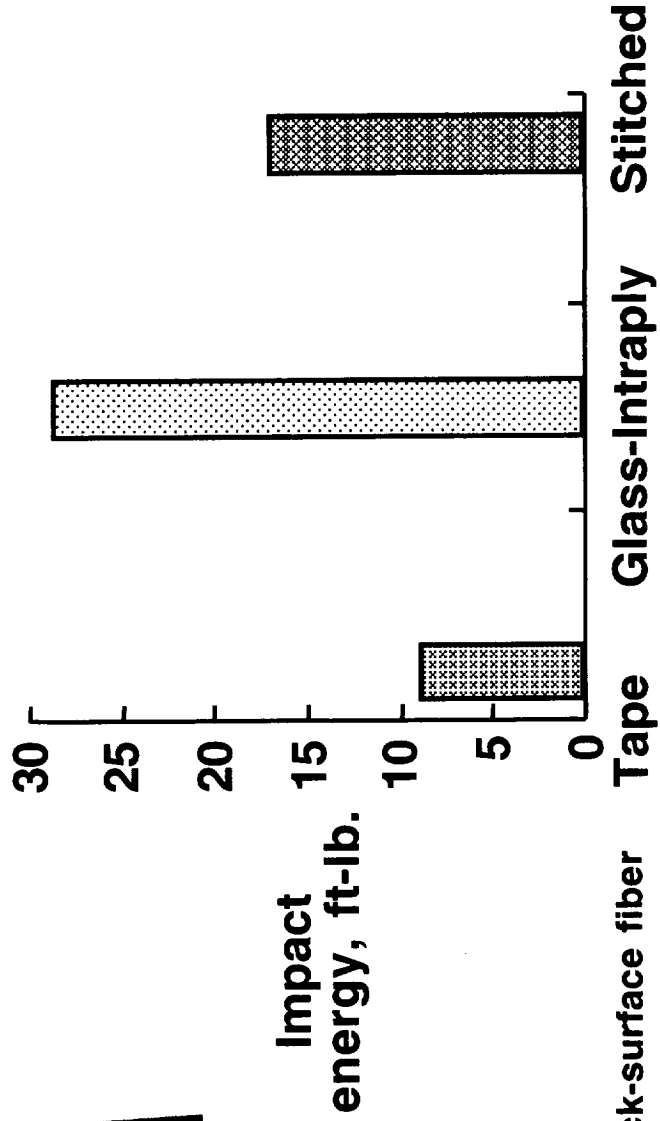
Pre-impregnated tape material



Graphite-glass intra-ply material



Back-surface fiber splitting



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PMC Damage Tolerance and Repair

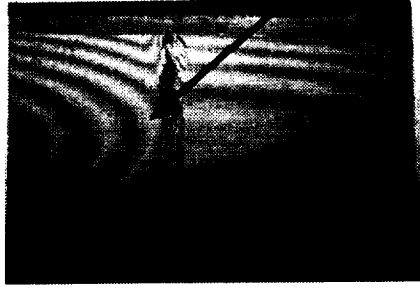
TYPICAL COMPRESSION RESPONSE AND FAILURE OF 16-PLY-THICK CURVED PLATES LOADED IN COMPRESSION

Displacement contour



Undamaged

Failed specimen



Failure location



Impact damaged



Impact damage location

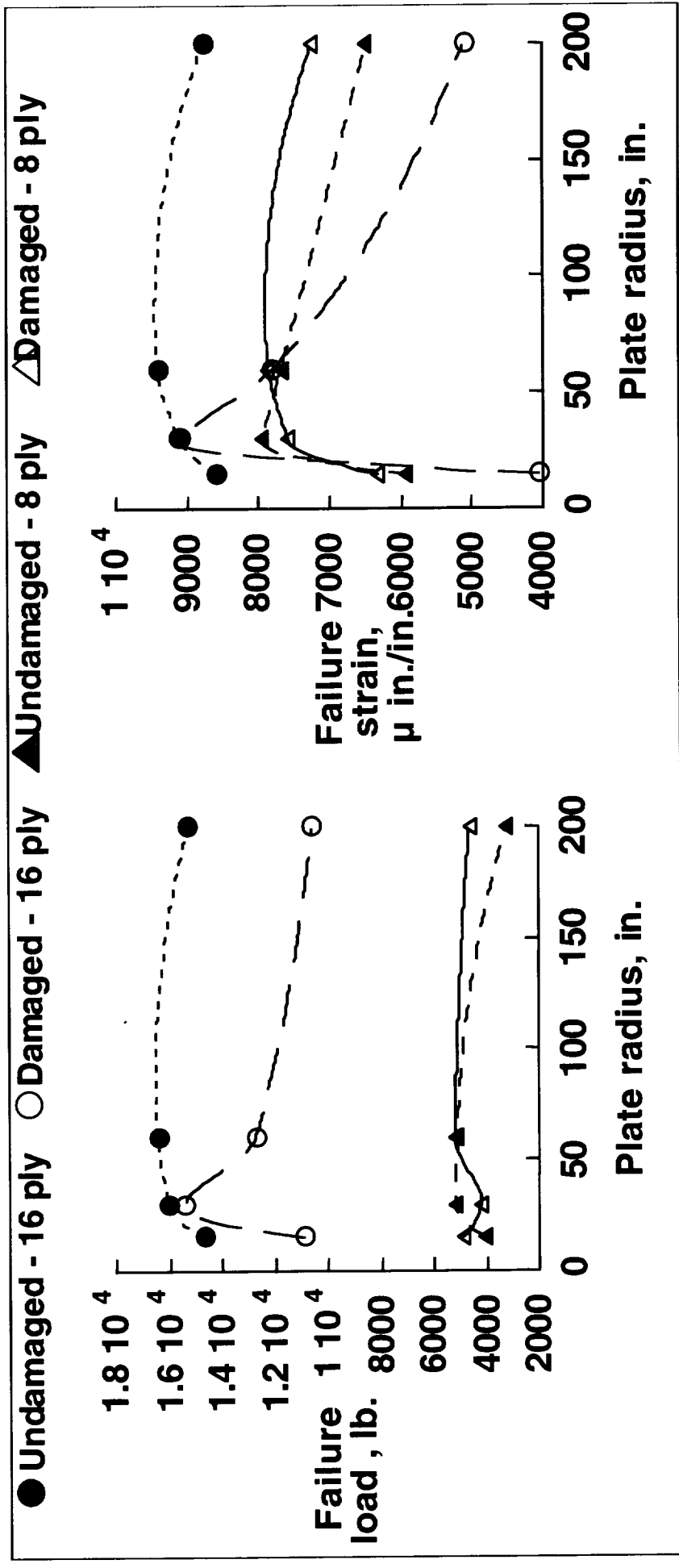
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COMPARISON OF COMPRESSION-AFTER-IMPACT STRENGTH RESULTS FOR CURVED THIN PLATES

AS4-3502 Prepreg Tape Material



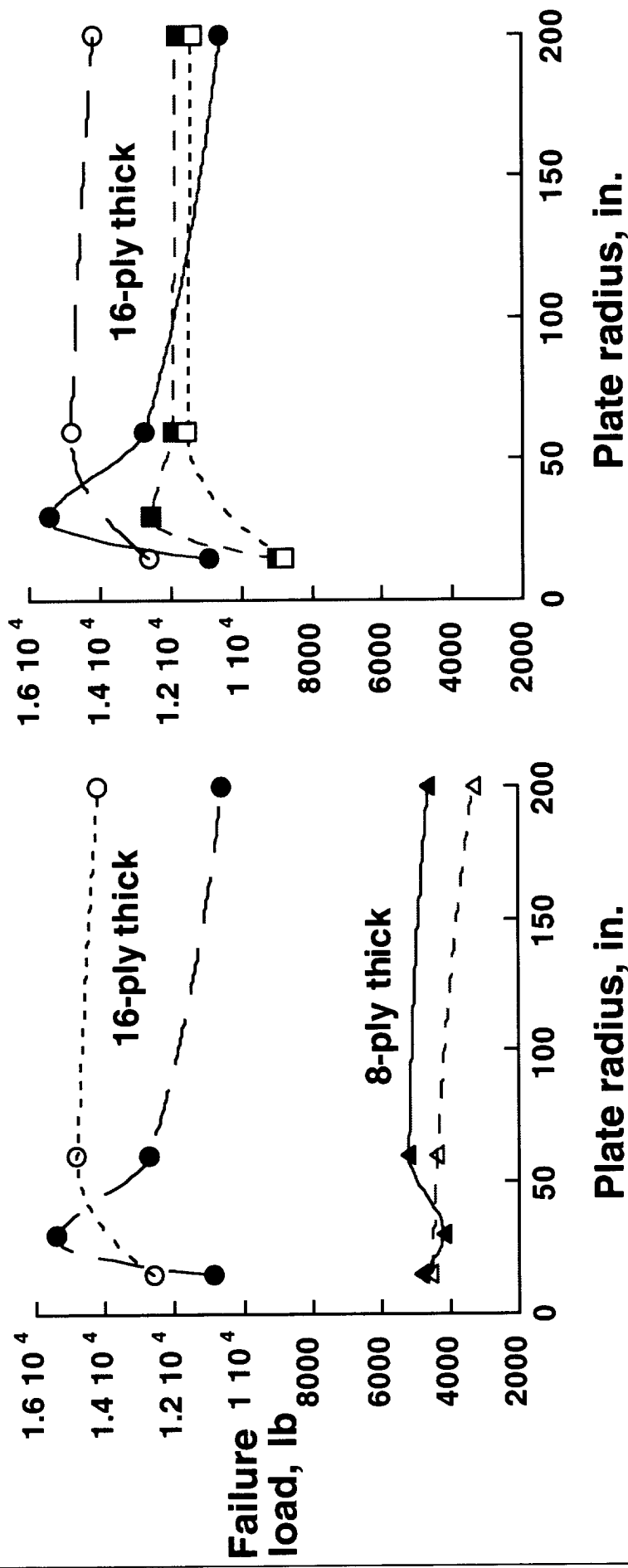
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COMPARISON OF RESIDUAL STRENGTH RESULTS FOR PLATES SUBJECTED TO DROPPED-WEIGHT IMPACT AND STATIC INDENTATION DAMAGE

- 2.5 lb impactor, 10 in. by 10 in. plate size ○ Static indentation, 10 in. by 10 in. plate size
- 2.5 lb impactor, 9 in. by 5 in. plate size □ Static indentation, 9 in. by 5 in. plate size
- ▲ 2.5 lb impactor, 10 in. by 10 in. plate size △ Static indentation, 10 in. by 10 in. plate size

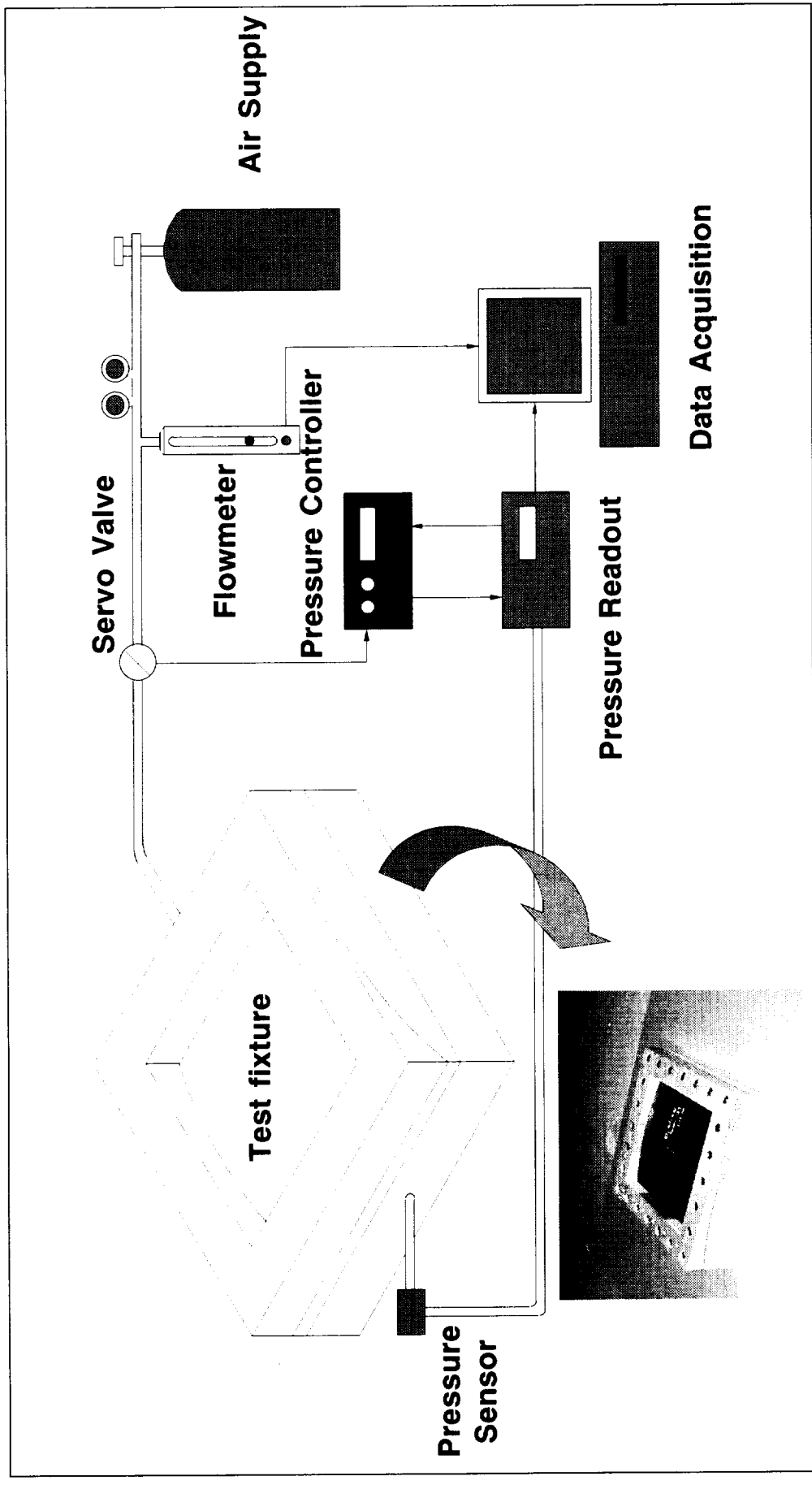


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SCHEMATIC DIAGRAM OF TEST SET-UP FOR PRESSURE LEAKAGE TESTS



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SUMMARY OF ANALYTICAL EFFORTS

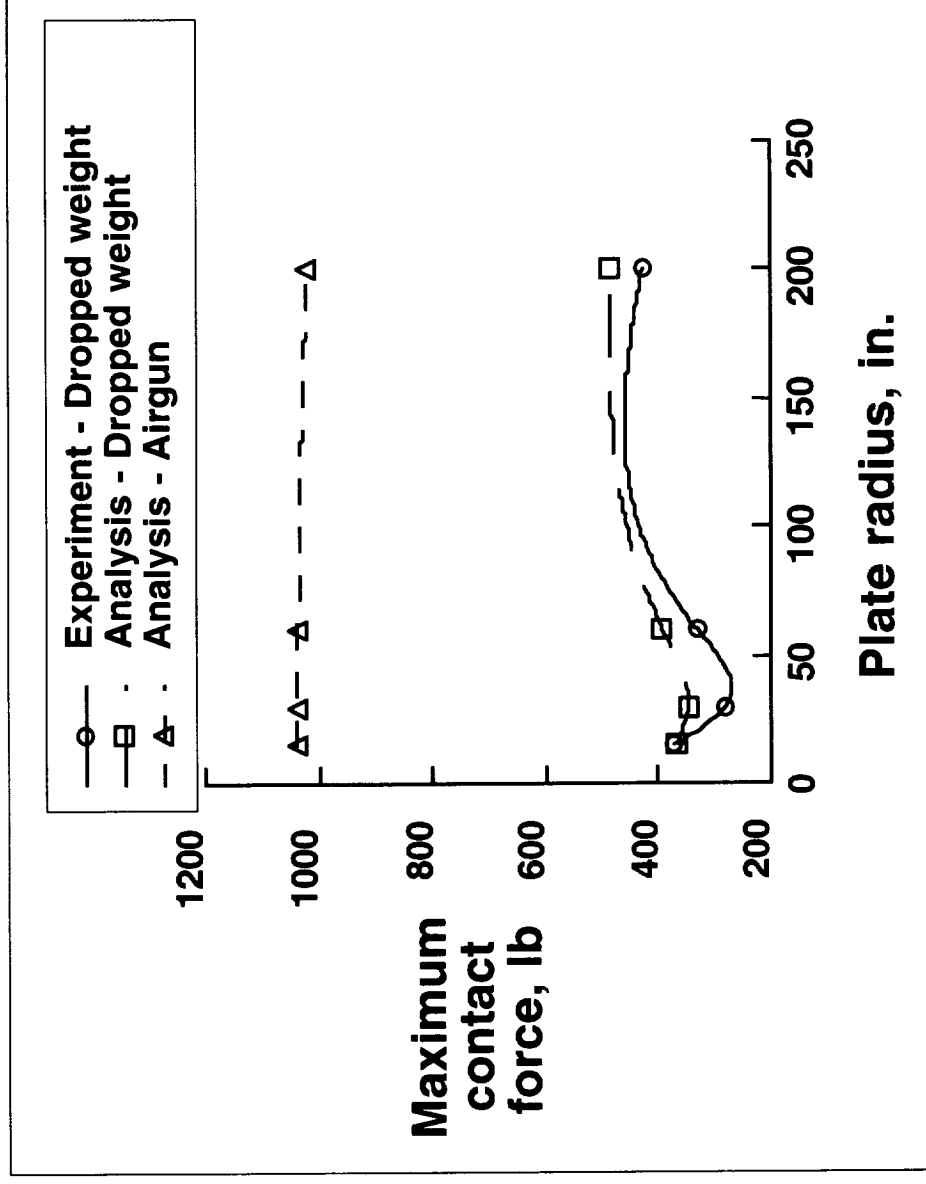
- ♦ **Impact response of thin curved laminates**
- ♦ **Finite element analysis to assess critical manufacturing defect size for combined mechanical and thermal loaded structures**
- ♦ **Methods for optimizing bonded and bolted repairs**

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DEVELOPED NONLINEAR ANALYSIS METHOD FOR ACCURATELY DETERMINING IMPACT RESPONSE AND DAMAGE INITIATION



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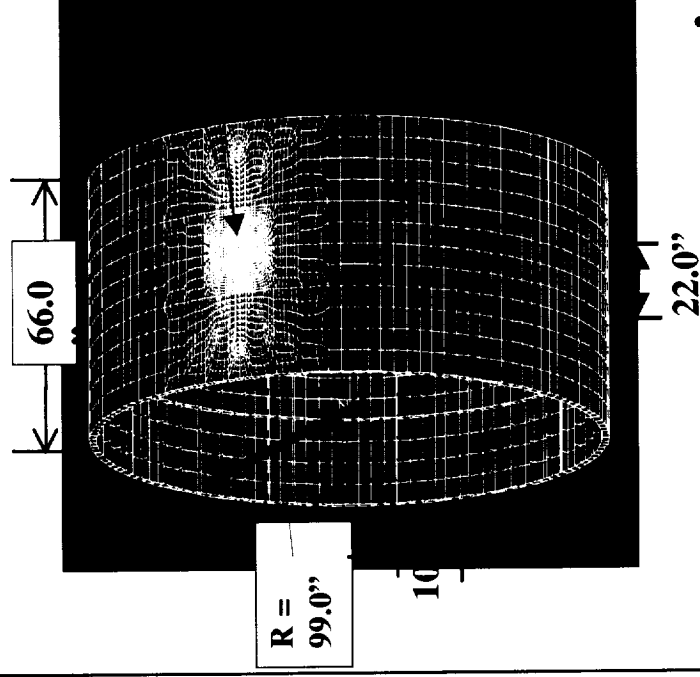
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DELAMINATION GROWTH STUDIES

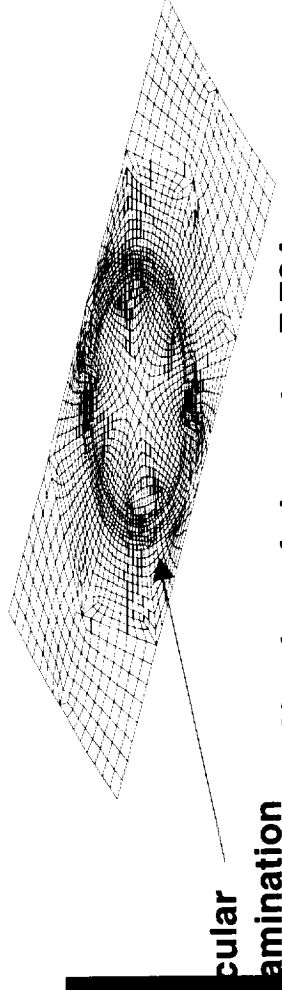
Modeling and Analysis Approach

Global model



- Number of elements: 10,664
- Dof: 64,314

Local model



- Number of elements: 7,784
- Dof: 46,548

Virtual crack closure technique to determine strain energy release rates.
Parametric studies with combined mechanical, thermal and internal pressure loading conditions.

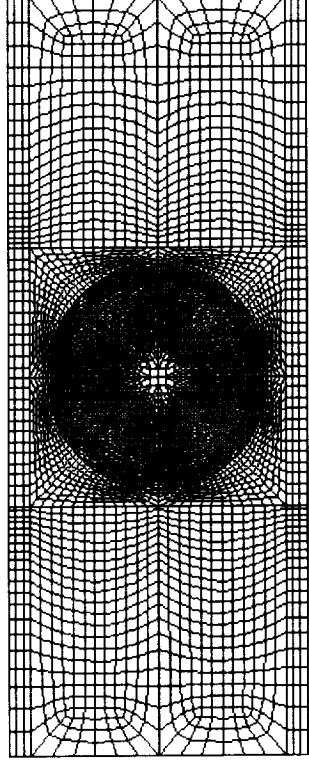
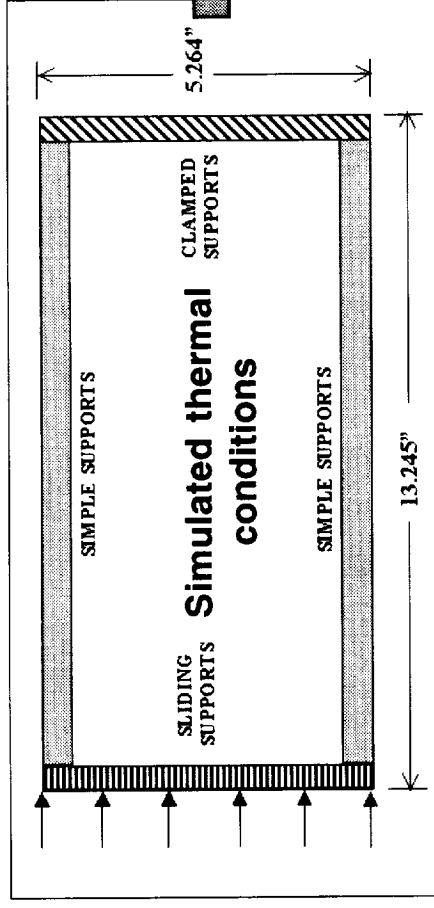
- Critical delamination size and location.
- Stiffened skin and sandwich constructions.

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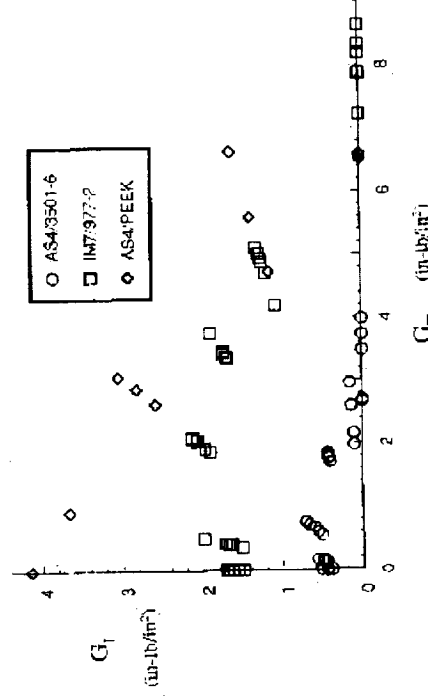
PMC Damage Tolerance and Repair

APPROACH FOR DELAMINATION GROWTH VERIFICATION TESTING



Finite element model

Test configuration



Fracture toughness data

Experimental verification
of the critical size and
location of delaminations

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NEAR-TERM PLANS

- ◆ **Conduct pressure leakage tests on laminates made from different material forms**
- ◆ **Complete compression-after-impact strength tests on laminates made from different material forms**
- ◆ **Complete delaminated panel compression tests at cryogenic temperatures to verify criticality of the effects of defects**

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- ♦ **PMC Damage Tolerance & Repair**
 - POC - Dr. Damodar R. Ambur/Dr. Tom S. Gates, NASA LaRC
- ♦ **Safe Structures Design Technologies**
 - POC - Dr. Damodar R. Ambur, NASA LaRC

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Safe Structures Design Technologies

Goals and Objectives

- ◆ Develop validated second generation nonlinear progressive failure analysis method for composite structures subjected to combined mechanical loads
- ◆ Develop non-deterministic analysis and design methods that bound manufacturing uncertainties
- ◆ Conduct sensitivity analyses for manufacturing uncertainties
- ◆ Develop and demonstrate 3rd. generation progressive failure analysis method that includes combined mechanical and thermal load effects and delaminations
- ◆ Develop design and analysis relationships between structural weight and reliability for composite structures subjected to combined mechanical and thermal loads
- ◆ Develop hybrid deterministic and non-deterministic analysis and design methods that account for uncertainties at the material, structures, and mission levels
- ◆ Conduct hierarchical sensitivity analyses and identify design trends for multiple length scales subjected to combined loads

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- ◆ **Current Program Status**
 - Initiated in FY2000
 - Efforts continue under the 3rd Generation RLV Program
- ◆ **Current Technical Status**
 - Developed analytical methods and algorithms for using the current damage progression methods to predict the response of nonlinearly deformed structures
 - Conducted progressive damage verification tests on a compression-loaded composite cylinder
 - Conducting progressive damage verification tests on a composite panel subjected to nonlinear deformation with in-plane shear loading
 - Initiated tools development for predicting delamination initiation and growth

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MECHANICS TECHNOLOGY FOR PROGRESSIVE FAILURE ANALYSIS

- ◆ Embed progressive failure criteria and material degradation models with robust nonlinear structural mechanics solver STAGS
- ◆ Provide progressive damage capability coupled with large displacement, large rotation deformation states for laminated composite structures
- ◆ Provide traditional and state variable damage models
 - Maximum strain with ply discounting
 - Crack density based criteria for failure and degradation
 - User interfaces include ABAQUS/UMAT
- ◆ Incorporate artificial damping feature to mitigate non-convergence problems in re-establishing equilibrium
- ◆ Establish consistency between first and second variations for the energy functional
- ◆ Enhance visual depiction of progressive damage simulation
- ◆ *Increased design robustness through evaluation of extreme loading conditions and understanding possible composite structures failure scenarios*

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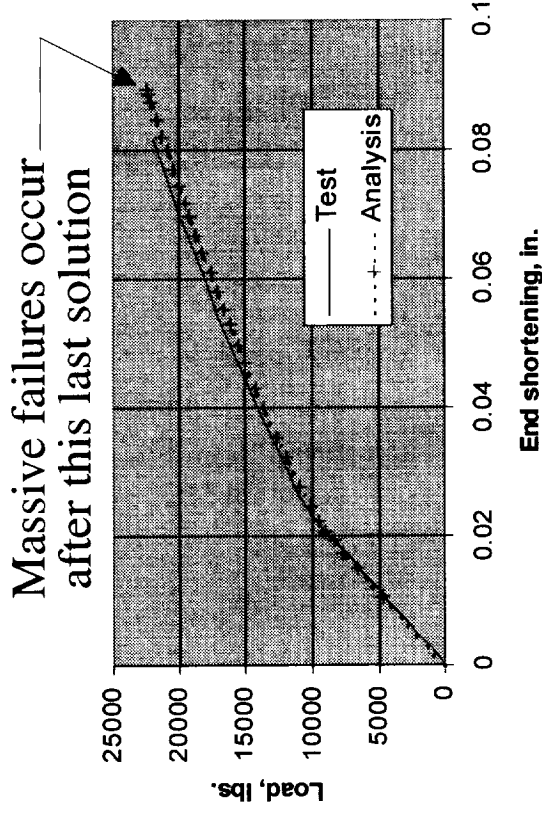
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COMPRESSION-LOADED POSTBUCKLING COMPOSITE PANEL

24-ply Graphite-epoxy
orthotropic laminate

Starnes & Rouse, AIAA
Paper 81-0543

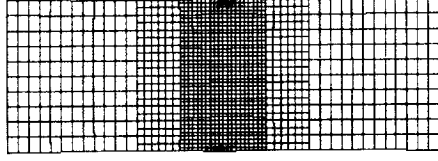
Failure load = 21,910 lbs
End shortening at failure
= 0.0818 in.



Out-of-plane
Deflections



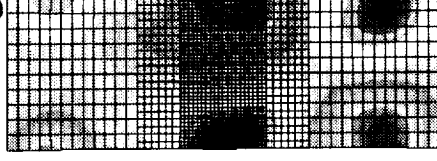
Percent Failed Plies



Close-up
of Failed
Region



Inplane Shear Stress in
Outer 0-deg. Layer



Close-up
Showing
Stress Relief

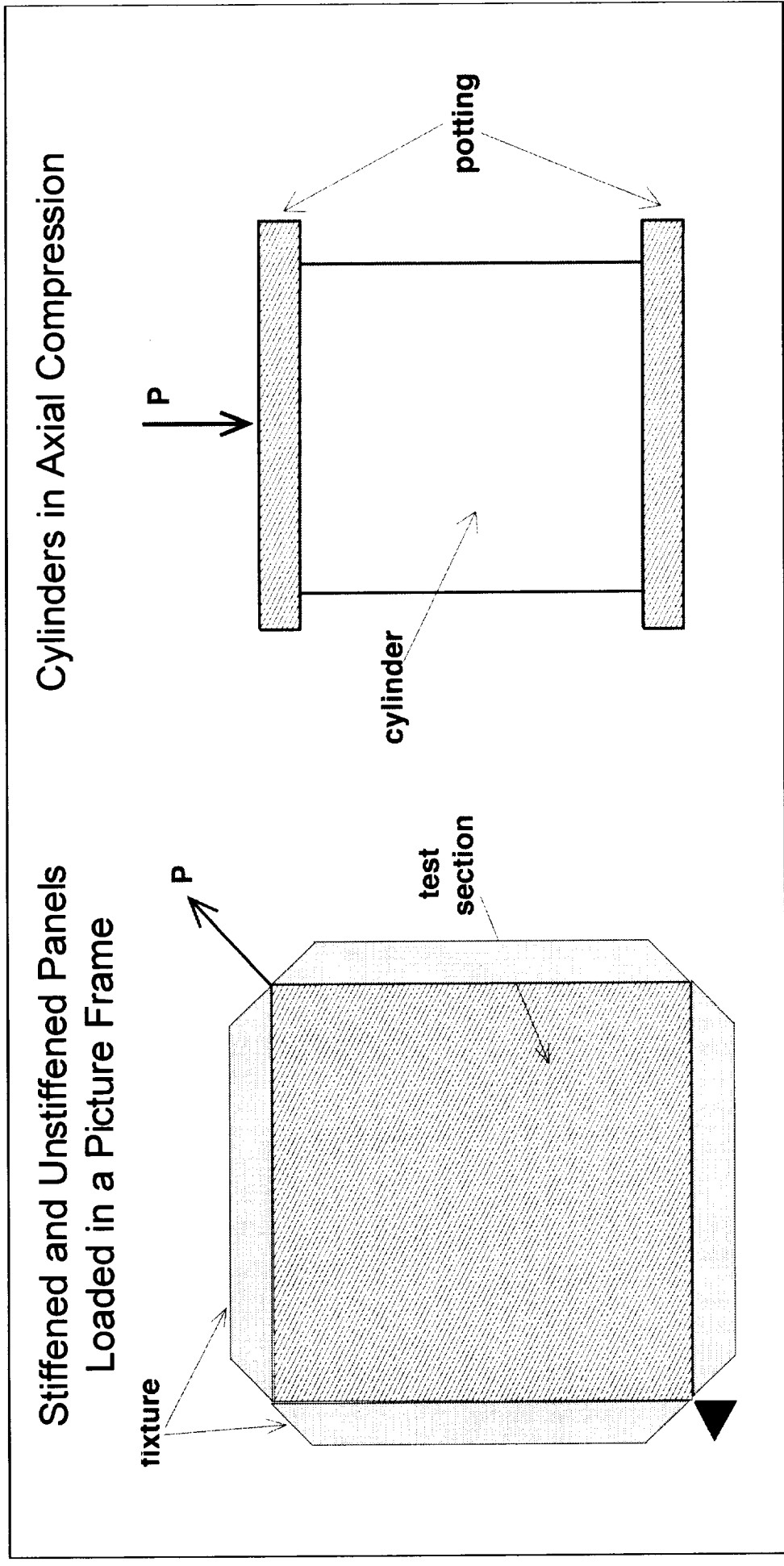


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CORRELATION OF PROGRESSIVE FAILURE ANALYSIS RESULTS FOR PANELS AND SHELLS



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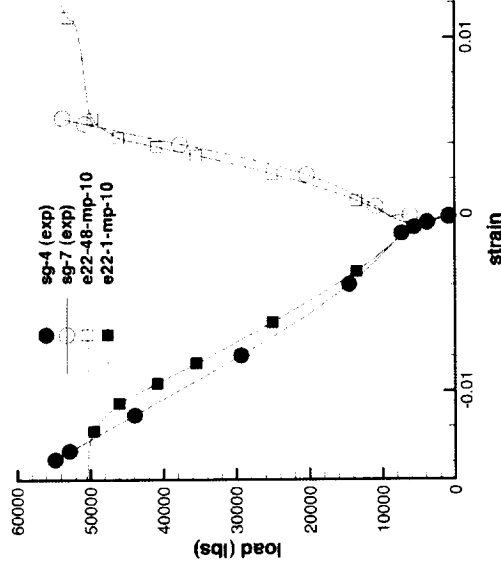
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UNSTIFFENED PANEL LOADED IN PICTURE FRAME SHEAR

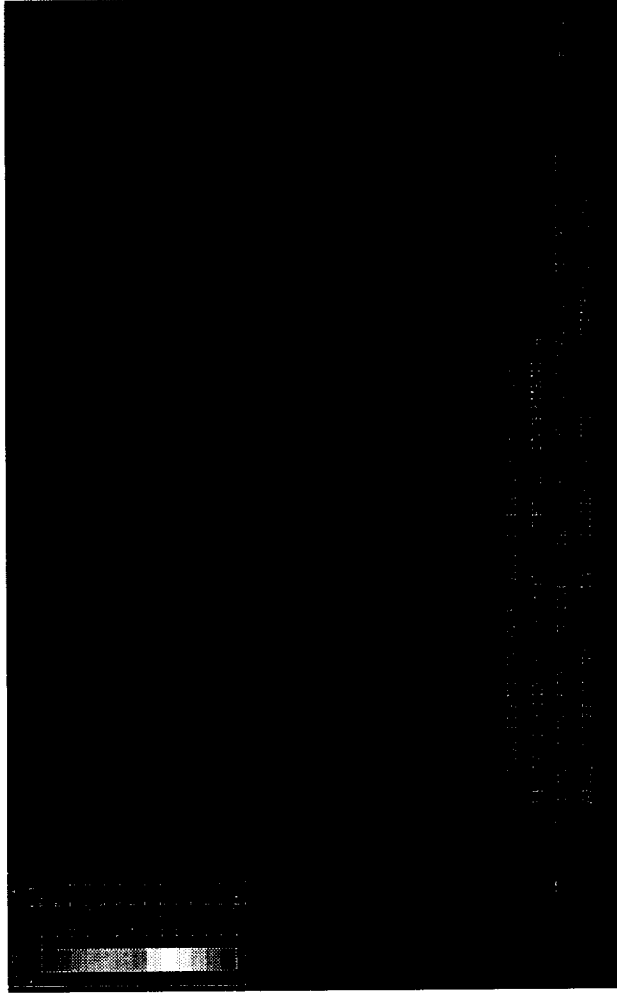
- Panel size: 12-in. by 12-in.; Thickness: 0.0896-in.
- Stacking sequence is $[\pm 45/0/90]_{2s}$
- $E_{11} = 18.5$ Msi, $E_{22} = 1.67$ Msi, $G_{12} = 0.87$ Msi, $G_{13} = 0.87$ Msi, $G_{23} = 0.258$ Msi, $\mu_{12} = 0.3$
- $X_T = 0.233$ Msi, $X_C = 0.21$ Msi, $Y_T = 0.0147$ Msi, $Y_C = 0.0287$ Msi, $SC = 0.02975$ Msi

Failure Load:
54,807 lbs - Test
54,447 lbs - Analysis

Strain Normal to Fiber Direction on Top and Bottom Surfaces at Center of Test-Section



Map of Matrix Failure Region



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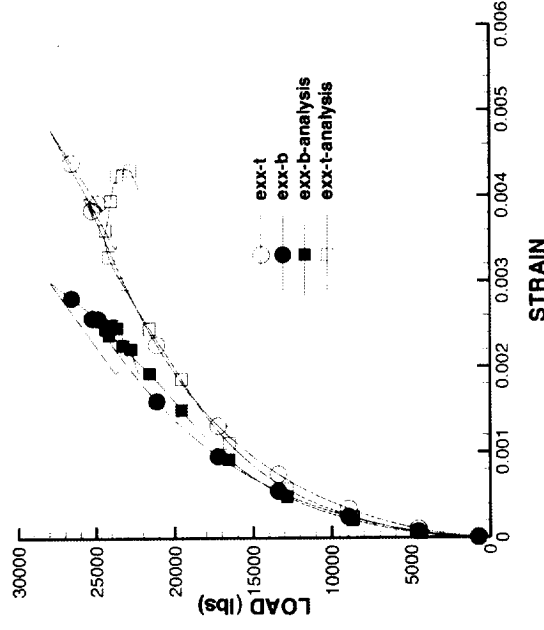
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BEAD-STIFFENED PANEL LOADED IN PICTURE FRAME SHEAR

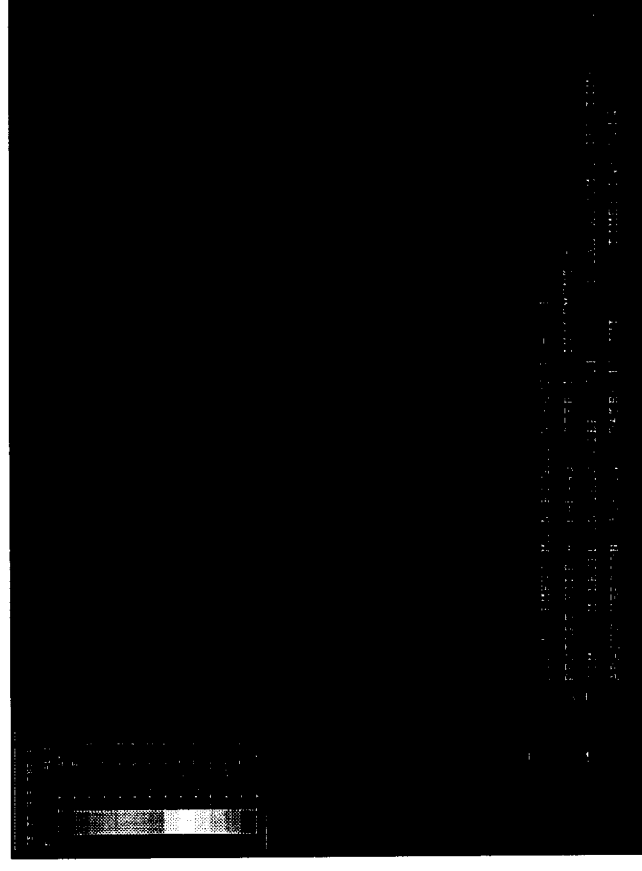
- Panel size: 12-in. by 12-in.; Thickness: 0.08-in.
- Stacking sequence is $[\pm 45/\pm 45/0/\pm 45/90]_s$
- $E_{11} = 18.0$ Msi, $E_{22} = 1.50$ Msi, $G_{12} = 0.82$ Msi, $G_{13} = 0.82$ Msi, $G_{23} = 0.82$ Msi, $\mu_{12} = 0.3$
- $X_T = 0.30$ Msi, $X_C = 0.20$ Msi, $Y_T = 0.013$ Msi, $Y_C = 0.031$ Msi, $SC = 0.027$ Msi

Failure Load:
27,936.9 lbs -Test
26,995.9 lbs -Analysis

Axial Strain on the Top and Bottom Surfaces at Center of Panel



Map of Matrix Failure Region



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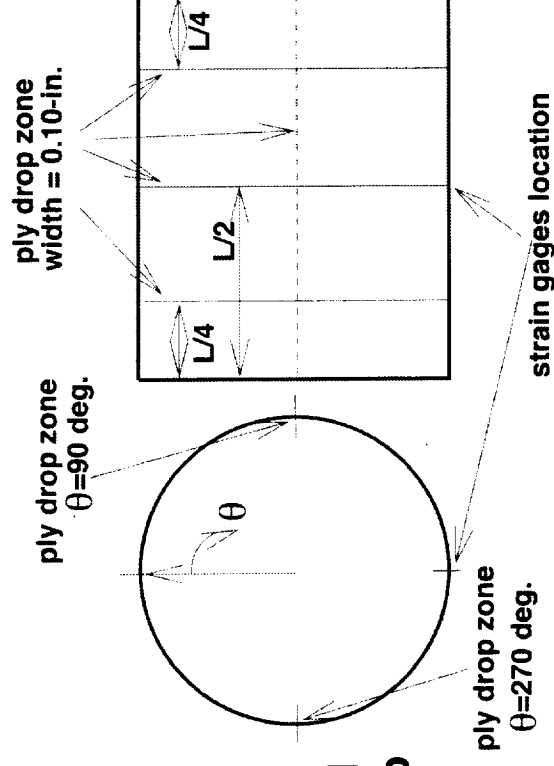
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EFFECTS OF MANUFACTURING UNCERTAINTIES ON COMPOSITE CYLINDER AXIAL COMPRESSION RESPONSE

- Cylinder is 16.0-in. long; 16.0-in. diameter
- Laminate is $[\pm 45/0/90]_{2s}$ and 0.08-in. thick
- $E_{11} = 19.0$ Msi, $E_{22} = 1.450$ Msi, $G_{12} = 0.814$ Msi, $G_{13} = 0.814$ Msi, $G_{23} = 0.55$ Msi, $\mu_{12} = 0.3$
- $X_T = 0.156$ Msi, $X_C = 0.156$ Msi, $Y_T = 0.00725$ Msi, $Y_C = 0.0145$ Msi, $SC = 0.010826$ Msi

• Two models were considered:

- Model 1:
 - Measured geometric imperfection modeled
 - 7,560 elements; 4-noded
- Model 2:
 - Measured geometric imperfection modeled
 - Laminate imperfection modeled as ply drop
 - 10,692 elements; 4-noded



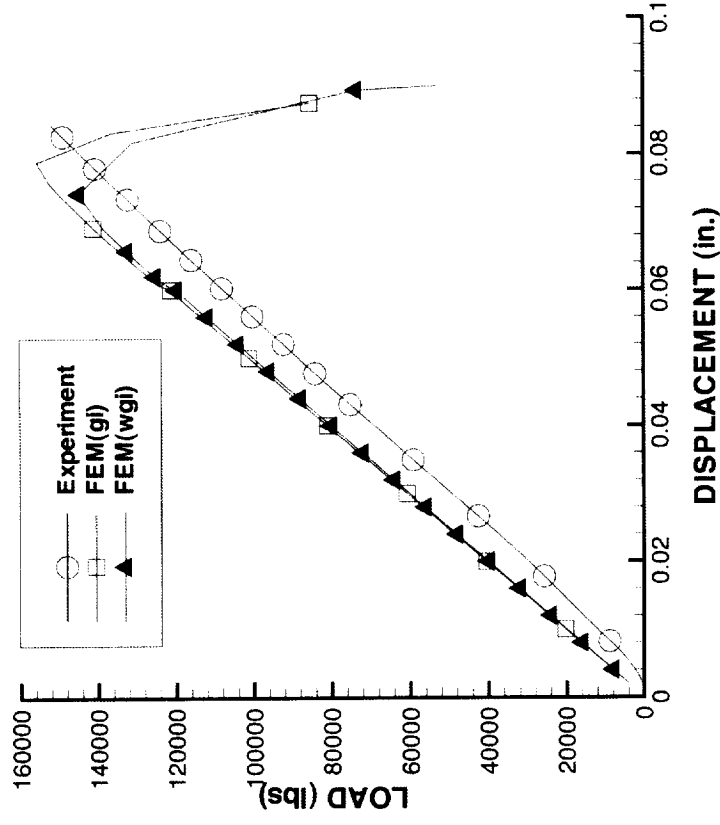
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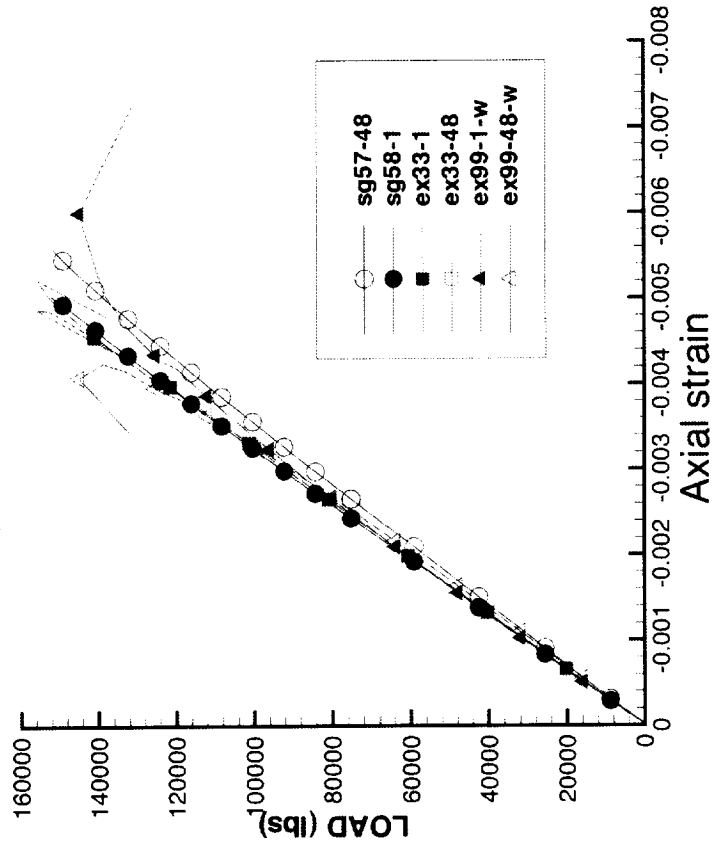
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EFFECT OF MANUFACTURING UNCERTAINTIES ON
COMPOSITE CYLINDER AXIAL COMPRESSION RESPONSE (Contd.)

Load Vs. End-shortening Results



Load Vs. Axial Strain Results



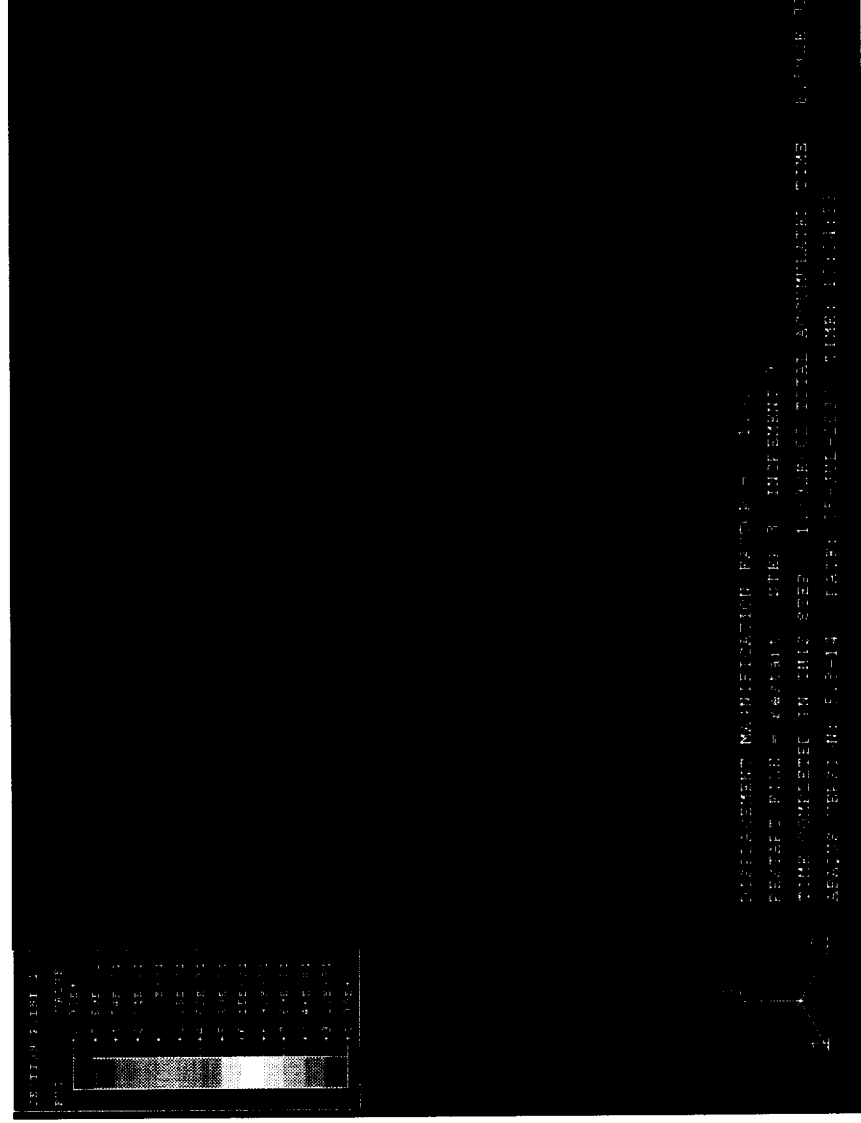
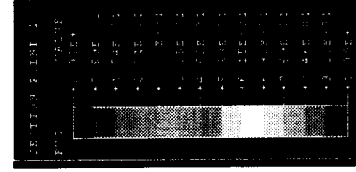
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EFFECT OF MANUFACTURING UNCERTAINTIES ON COMPOSITE CYLINDER AXIAL COMPRESSION RESPONSE (Contd.)

Map of Failure Region for Model 1



Failure Region

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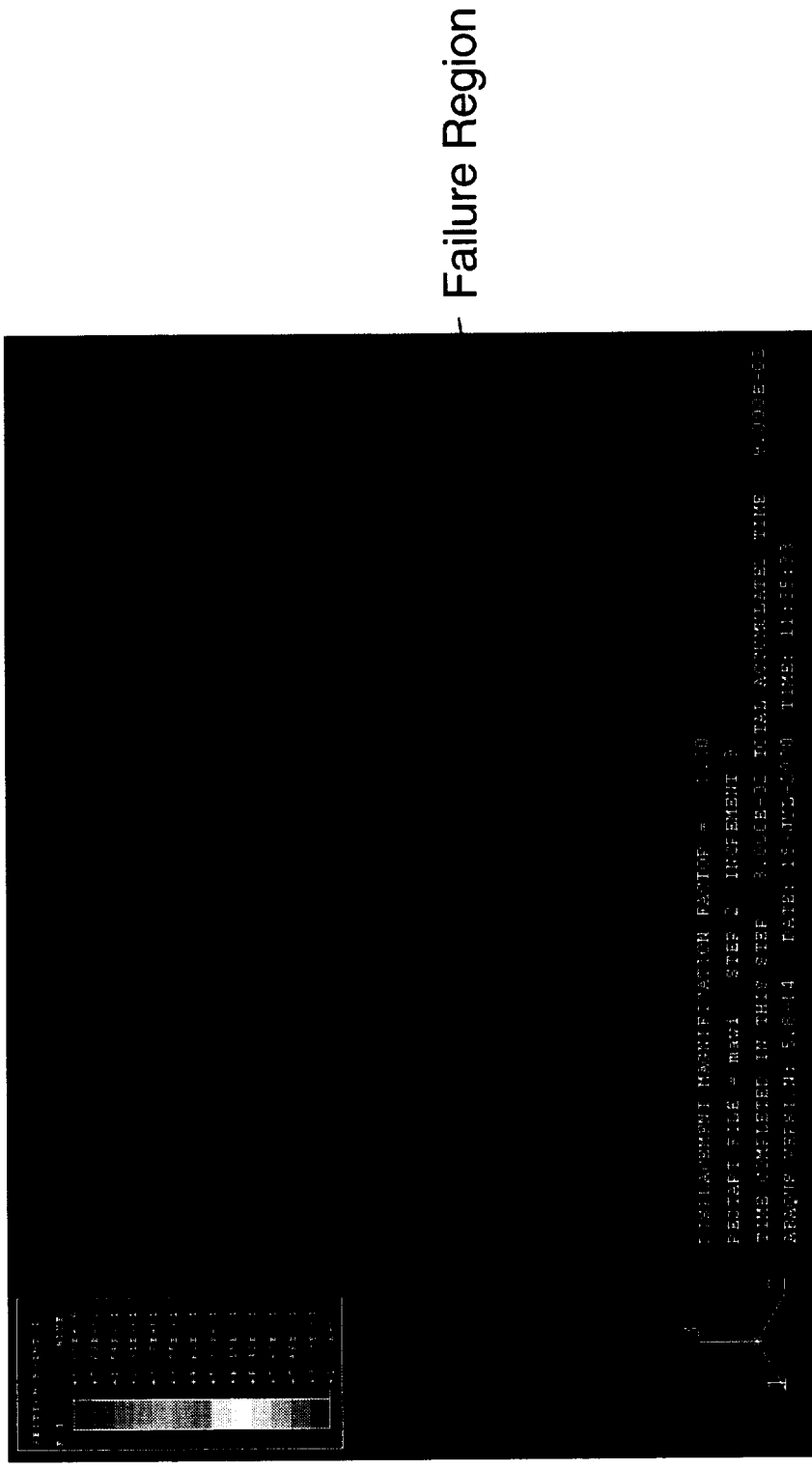
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EFFECT OF MANUFACTURING UNCERTAINTIES ON

COMPOSITE CYLINDER AXIAL COMPRESSION RESPONSE (Concluded)

Map of Failure Region for Model 2

Failure modes and damage region results obtained using Model 2 compare well with experimental results



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NEAR-TERM PLANS

- ◆ Conduct inplane shear tests on stiffened and unstiffened panels
- ◆ Correlate analytical and experimental results
- ◆ Continue efforts to validate the decohesion element for simulating the delamination failure mode
- ◆ Incorporate decohesion element into STAGS finite element analysis code

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